Improved Energy Efficiency in Paper Making by Reducing Dryer Steam Consumption Using Advanced Process Control

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Synopsis

• The energy used in paper making
• The need for multivariable process control: Advanced Process Control
• Reduction in the energy used in paper making: some dryer steam reduction results from recent APC implementation projects
  - **Board making:** >10% energy reduction to date + consequent production benefit
  - **Newsprint:** also >10% energy reduction to date
• Towards further reduction of dryer steam use: results from current paper machine investigations of the potential for dryer steam reduction
  - by better control of drainage
  - by optimisation of the dryer hood
• Case study material from several paper machines:
  - Two ply board machines in England and Australasia
  - Newsprint machines in England and in North America
• Conclusion
The Energy Used in Paper Making

- Paper-making is a very energy-intensive industrial activity. UK 2008 figures:

<table>
<thead>
<tr>
<th>Paper Type</th>
<th>Energy Consumed</th>
</tr>
</thead>
<tbody>
<tr>
<td>Packaging board</td>
<td>2 – 3 MWhr/t paper made</td>
</tr>
<tr>
<td>Newsprint</td>
<td>3 – 4 MWhr/t</td>
</tr>
<tr>
<td>Tissue</td>
<td>5 – 7 MWhr/t</td>
</tr>
<tr>
<td>Fine Papers</td>
<td>4 – 8 MWhr/t</td>
</tr>
<tr>
<td>Specialty papers</td>
<td>Up to 20 MWhr/t</td>
</tr>
<tr>
<td><strong>UK Average</strong></td>
<td><strong>4 MWhr/t</strong></td>
</tr>
</tbody>
</table>

- Energy was cheap & plentiful when present day pulp & paper industry processes were designed:
  - About 70 paper machines are still operated in the UK but >200 operated 50 years ago
  - Each machine costs £10s of millions each; not easy to change technology fast
- The rising cost of energy has shut more than 10 UK paper mills in the last three years; this picture is reflected elsewhere in the Northern Hemisphere
- Thus there are strong incentives to reduce the energy used in paper making
Energy Use on the Paper Machine

- Paper machines use between 50% and 80% of mill energy (when there are no pulp mills on site)
- Some of this is electrical energy used in drives and in running vacuum pumps and stock pumps (for moving fluids)
- But steam used in drying the sheet is the biggest energy consumer
- Water content of the sheet:
  - when sheet is just formed, 99.1% is water: vacuums and aerofoils drain it
  - as it enters the press section the sheet is ~88% water
  - as it enters the dryer the sheet is ~50% water: steam is used to dry the sheet to ~8% water content
Dryer Steam: the Big Energy User in Paper Making

It is known that the drying section of a paper machine:
• reduces sheet moisture content, M, from ~50% to ~ 8% \( M = \frac{\text{water}}{\text{water} + \text{fibre}} \)
• uses up to 80% of mill-wide energy
• but removes less than 1% of water from the sheet

Consider 100 gm of thin stock laid onto the wire at the headbox:
• 0.9 gm total solids
• 99.1 gm water
At the dryer, M ~ 50%:
• there is still 0.9 gm solids
• and just 0.9 gm of water
• 98.2 gm of water have been removed
• less than 1 gm of water remains to be removed through the whole of the dryer.
Effect on Dryer Steam Use of Decreasing Sheet Moisture Content at Dryer Entry

- Take headbox consistency as 0.9% and consider the fate of 100g of stock laid on the wire. Using $M = \frac{\text{mass of water in sheet}}{(\text{mass of total solids} + \text{mass of water})}$

<table>
<thead>
<tr>
<th></th>
<th>At the headbox</th>
<th>At the couch</th>
<th>Into the dryer</th>
<th>Better dryer feed</th>
<th>At the reel</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sheet moisture M</td>
<td>99.1%</td>
<td>88%</td>
<td>50%</td>
<td>45%</td>
<td>8%</td>
</tr>
<tr>
<td>Water in sheet</td>
<td>99.1g</td>
<td>6.6g</td>
<td>0.9g</td>
<td>0.736g</td>
<td>0.078g</td>
</tr>
<tr>
<td>Solids in sheet</td>
<td>0.9g</td>
<td>0.9g</td>
<td>0.9g</td>
<td>0.9g</td>
<td>0.9g</td>
</tr>
<tr>
<td>Water removed</td>
<td>92.5g</td>
<td>5.7g</td>
<td>5.86g</td>
<td>0.822 (0.658g)</td>
<td></td>
</tr>
</tbody>
</table>

- Wire drains over 92% of water, press drains <6%, dryer removes <1% !!
- If can ↓ sheet moisture to the dryer by 5%, water to be removed in the dryer ↓ from 0.822g to 0.658g. A 5% ↓ in sheet moisture => 20% ↓ in dryer load ie
- “A 1% reduction in sheet moisture to the dryer yields a 4% reduction in dryer load”
Ways to Reduce Dryer Steam Use in Paper Making

Dryer steam use constitutes up to 80% of the energy used in making paper => interest in determining opportunities to reduce dryer steam use:

• **Reduce the incidence of over-drying of the sheet**
  - A 1% increase in sheet moisture content ↓ dryer steam demand by 1.34%

• **Reduce the incidence of over-weight making of the sheet**
  - A 1% reduction in sheet weight reduces dryer steam demand by 1.034%

• **Increase drainage of the sheet before it enters the dryer:**
  - A 1% reduction in sheet moisture entering the dryer delivers a reduction in dryer steam demand of 4%: a very useful magnification factor!

• **Improve dryer efficiency:** measuring dryer efficiency in terms of mass water evaporated/mass of steam used
  paper dryers are typically ~50% efficient. Opportunities to improve this:
  - Better regulate and optimise the operation of the dryer hood
  - Use all available variables for control of sheet drying: for each dryer section use
    • Differential pressures as well as supply steam pressures
    • Condensate recovery rates – where these are separately manipulable
Advanced Process Control in Paper Making

• Most processes in the pulp & paper industry are strongly multivariable
• Control problems in the paper industry require multivariable solutions:
  - A paper machine has many unused control variables because it has never been clear how to use them in a PID control law eg
  • Formation and drainage are jointly affected by the same input variables, often >15 of them
  - Key quality variables are often controlled using a PID loop that adjusts just one of several variables affecting the quality variable eg
  • Recycled pulp brightness: controlled by bleach rate alone (expensive), ignoring other influences on brightness uplift
• Advanced Process Control (APC) offers optimal multivariable Model-based Predictive Control (MPC) subject to specified constraints:
  - profit can often be made by operating close to or at constraints
  - why control a tank level to a setpoint (as with PID) when what is required is simply to keep the tank from over-flowing or under-flowing
• APC was developed in oil & petrochem – still quite new in the paper industry
Advanced Process Control: Some Important Characteristics

- Need first to build a multivariable process model: the model describes how each input affects all the outputs
- There can be a model for each grade range
- Can specify constraints on each input and on each output
- In pulp & paper, operating priorities can change hour by hour => need real-time optimisation: can run APC with optimisers to determine optimal setpoint targets within the specified constraints
- Every application has given considerable performance improvement: APC provides a step change in control technology
- We have engineered successful APC applications on most p&p processes: project payback times to date have been between 0.5 and 9 months
Energy Reduction in Paper Making Using APC: Some Recent Results

- The following results arise from APC implementations on paper machines making board and paper machines making newsprint.
Reduced Energy Consumption in Paper Making: The Role of Wet End Stability Improvement

• To optimise and better control energy use in paper making, a necessary first step is often to improve wet end stability.
• White water consistency, retention, ash content, formation and drainage are all affected by a number of stock approach and machine variables, many having an impact on energy use in paper making:
  - refiner specific energy targets
  - the flowrates & consistencies of fresh stock, broke and recovered fibre
  - the dosage rates of wet end chemicals, including retention aids & fillers
  - headbox parameters such as slice gap and jet to wire ratio
  - wire vacuums
• APC Objective: maintain stability of white water consistency, retention, ash content and other quality parameters to provide a platform from which to be able to optimise drainage in order to minimise energy use.
• Multivariable model-based control tools are very well suited to this multi-dimensional control and optimisation problem.
Performance Improvement in Paper Making: 1. Multi-Ply Board Machines

- Design objectives for an APC implementation on an Australasian 2-ply board machine making 100 – 220 gsm products:
  - Improve machine stability
  - Reduce energy usage
  - Increase production

- Many board machines are dryer-bottlenecked => reducing steam consumption can have three benefits:
  - Lowers cost of paper production by reducing specific energy consumption
  - Less steam needed/tonne => more tonnes possible: increased production
  - Drier sheet => improved runnability and faster average speeds
Australasian Board Machine: Stability Results

- There was a big reduction in variation:
  - standard deviations of wet end parameters reduced by between 75% & 90%.
  - reductions in SDs of WWC: TL by 82% and BL by 73%:
### Australasian Board Machine: Steam Saving >10%

<table>
<thead>
<tr>
<th>Grade (GSM)</th>
<th>Steam Consumption (t/t) under Regulatory Control</th>
<th>Steam Consumption (t/t) under APC</th>
<th>% Reduction in Steam Use</th>
</tr>
</thead>
<tbody>
<tr>
<td>108</td>
<td>2.17</td>
<td>2.11</td>
<td>2.92</td>
</tr>
<tr>
<td>115 A</td>
<td>2.53</td>
<td>2.23</td>
<td>11.99</td>
</tr>
<tr>
<td>115 B</td>
<td>2.31</td>
<td>1.90</td>
<td>17.75</td>
</tr>
<tr>
<td>120</td>
<td>2.22</td>
<td>2.00</td>
<td>9.93</td>
</tr>
<tr>
<td>150</td>
<td>2.24</td>
<td>2.19</td>
<td>2.22</td>
</tr>
<tr>
<td>140</td>
<td>2.24</td>
<td>2.01</td>
<td>10.02</td>
</tr>
<tr>
<td>200</td>
<td>2.24</td>
<td>1.71</td>
<td>23.67</td>
</tr>
<tr>
<td><strong>Average</strong></td>
<td><strong>2.24</strong></td>
<td><strong>1.71</strong></td>
<td><strong>23.67</strong></td>
</tr>
</tbody>
</table>

- How? APC uses flowrate of drainage aid (cheaper) preferentially to retention aid in controlling white water stability => increased drainage flowrates & reduced variation in drainage flowrates at the former:

<table>
<thead>
<tr>
<th>Suction Box</th>
<th>APC SD (l/min)</th>
<th>Regulatory SD (l/min)</th>
<th>% Reduction in SD</th>
</tr>
</thead>
<tbody>
<tr>
<td>Former Flow 1</td>
<td>177.2</td>
<td>265.1</td>
<td>33.2</td>
</tr>
<tr>
<td>Former Flow 2</td>
<td>55.7</td>
<td>68.5</td>
<td>18.7</td>
</tr>
</tbody>
</table>

- Mill now focussing on further improvements in drainage: effect of vacuums & headbox parameters on drainage (current project, reported later)
Australasian Board Machine: Better Quality & Production Increase

• Reduced variation in MD weight & moisture: though the controller was focussed on improving wet end stability alone:
  - The standard deviation of MD Basis Weight was reduced by 19.8%
  - The standard deviation of MD Moisture was reduced by 14.1%
• Production benefits due to:
  - improvements in runnability
  - reduction of the dryer bottleneck (by reducing specific steam consumption)
  gave a production increase in excess of 5.5%

- Design objectives for an APC implementation on a North American newsprint machine:
  - Improve machine stability
  - Reduce energy usage
  - Improve colour control
  - Reduce variation in sheet ash

- Multivariable structure of the controller:
North American Newsprint Machine: Stability and Ash Results

- The standard deviation of white (tray) water consistency was reduced by ~60%:
  - APC not active
  - APC Active

- APC reduced the standard deviation of the sheet ash content by > 50% =>
  - can run higher sheet ash contents and save fibre
**North American Newsprint Machine: Energy Saved >10%**

<table>
<thead>
<tr>
<th>Grade</th>
<th>Normal</th>
<th>ControlMV</th>
<th>%Change</th>
</tr>
</thead>
<tbody>
<tr>
<td>45A</td>
<td>1.820</td>
<td>1.600</td>
<td>12.1</td>
</tr>
<tr>
<td>45B</td>
<td>1.835</td>
<td>1.674</td>
<td>8.8</td>
</tr>
<tr>
<td>48A</td>
<td>1.858</td>
<td>1.613</td>
<td>13.2</td>
</tr>
<tr>
<td>48B</td>
<td>1.854</td>
<td>1.688</td>
<td>8.9</td>
</tr>
<tr>
<td>52A</td>
<td>1.894</td>
<td>1.745</td>
<td>7.9</td>
</tr>
<tr>
<td>52B</td>
<td>1.825</td>
<td>1.649</td>
<td>9.6</td>
</tr>
<tr>
<td>Averages</td>
<td>1.848</td>
<td>1.662</td>
<td>10.1</td>
</tr>
</tbody>
</table>

- Recent discussions about extending the controller have focussed on:
  - better control of drainage to further reduce dryer steam consumption
  - better control of the dryer and sheet moisture
  - control of luminance/brightness by optimising the use of bright clays, in conjunction with the improved ash control APC has provided
North American Newsprint Machine: Colour Results

We have reduced the SD of A*/B* colour by an average of 66%:

<table>
<thead>
<tr>
<th></th>
<th>Normal</th>
<th>MPC</th>
<th>% Change</th>
</tr>
</thead>
<tbody>
<tr>
<td>A*</td>
<td>0.088</td>
<td>0.039</td>
<td>58.6</td>
</tr>
<tr>
<td>B*</td>
<td>0.158</td>
<td>0.043</td>
<td>73.1</td>
</tr>
<tr>
<td>Average</td>
<td>0.123</td>
<td>0.041</td>
<td>65.8</td>
</tr>
</tbody>
</table>
Towards Further Reduction of Energy Use in Paper Making: Better Control of Drainage

• Better control of drainage =>
  - Optimise vacuum power and steam saving, maximise solids content of sheet entering dryer => reduce dryer steam use (1% ↓ in moisture => 4%↓ in steam)
  - Provide better control of sheet moisture

• Many influences on sheet drainage: amount of refining, rate of use of chemical additives (especially drainage aids), stock consistencies, headbox parameters, vacuums imposed, press pressures (current project)

• All of these variables affect other sheet properties than moisture alone => multivariable control can provide coordinated control of drainage and other quality and production variables

• Thus, more intelligent control of drainage can have simultaneous energy reduction and quality improvement objectives resulting in:
  - Reduced steam usage in the dryer, by draining to lower moisture contents
  - Steadier sheet MD moisture profiles
  - Hence steadier draw in the press section
  - Better control of formation (if measured online)
Overview of a Recent Drainage Study on a Two-Ply Board Machine

- **Purpose**: determine the influence of a comprehensive set of wet-end, headbox and wire-section variables on drainage and sheet moisture.

- **Sensors** had been installed to measure sheet solids content online at 3 wet end locations: pre-former, post-former, pre-couch.

- **Study Objectives**:
  - Identify which wire-section vacuums have an influence on drainage and what that influence is.
  - Determine which other wet-end and headbox variables also affect drainage.
  - Apply process response tests to the variables and develop a process model from this data.
  - Recommend which of the non-automated vacuums should be automated.
  - Suggest optimal settings for vacuums at the forming table and the former to maximise sheet dryness.
  - Using either regulatory or Advanced Process Control techniques, provide suggestions for a process control strategy for these vacuums and the wet end and headbox variables that are found to influence drainage.
Audit Methodology

- Data was collected by the board machine’s APC system, ControlMV.
- Process response tests were applied to 35 key wet-end/wire-section variables.
- Data analysis, correlation, process modelling and simulation was completed using Perceptive Engineering’s offline development package, ArchitectMV.
- Correlation matrix displays were used to determine nature of process interactions.
- Later slides show some representative examples of process behaviour.

The coloured boxes represent the strength of the relationship and the time delay.

**GOOD**
- Dark Blue – Strong with time delay.

**BAD**
- Light Blue – Weak with time delay.
- Dark Green – Strong/ incorrect delay.
- Light Green – Weak/incorrect delay.

The “cause” is the variable being tested.
Operational Data: BL Vacuum Operational Data

1. During period “A” the wire-section is set up with high vacuum...

2. Pre-former dryness is high, post and couch former dryness is low.

3. In period “B”, the vacuums were reduced dramatically. The wet/activity line is close to the former lead roll.

4. In response, pre-former dryness drops but pre-couch roll dryness increases.

5. At the position marked by the arrow the drive connection was enabled. When the vacuums are intensified again in period “C” there is a 5% increase in drive power consumption.
Operational Data: The Influence of Freeness

2. As °SR reduces, drainage improves, dryness increases and consequently steam consumption drops.

3. Conversely, as °SR increases, dryness drops and steam consumption increases.

4. The former responds in an unexpected way. With good drainage, the total former flow drops!

5. The flow in the 2nd compartment reduces (a lot) and flow in the 3rd comp increases (slightly).

This observation suggests that when drainage is good, the forming table is removing proportionately more water than the former.

1. At this position we have relatively high °SR, but it is reducing.
Process Response Tests
A Particular Post-Former Vacuum

1. The AMK012 vacuum control was tested in manual after the former.

2. The steps have a massive effect on couch roll dryness.

3. However, they do nothing to sheet moisture. This appears to give evidence of the press-section buffering out drainage changes after the former.

The correlation matrix confirms this. Basically no effect on sheet moisture. Very strong correlations on all other variables.
Process Response Tests
Two Particular BL Vacuum Boxes

In this area we can see the relationship between dryness and °SR (the two purple trends).
Process Response Tests
One BL Vacuum Box in more detail

- This response data suggests perhaps that too much vacuum on the forming table “seals the sheet”….

An increase in vacuum:
- Raises the drive roll current.
- Increases pre-former dryness.
- Decreases couch dryness.
- Increases moisture.

All bad news!
Process Response Tests
A Particular TL Box

- There is no correlation between the individual TL boxes and dryness, with the exception of box 15 (whose vacuum is separately supplied)
- Box 15 has a correlation to couch roll dryness and wire section power

### Abs. Effects

<table>
<thead>
<tr>
<th>Abs. Causes</th>
<th>TW Vacuum Box 15</th>
</tr>
</thead>
<tbody>
<tr>
<td>TW Vacuum Box 15</td>
<td></td>
</tr>
<tr>
<td>TW Vacuum Box 11</td>
<td></td>
</tr>
<tr>
<td>TW Vacuum Box 10</td>
<td></td>
</tr>
<tr>
<td>TW Vacuum Box 13</td>
<td></td>
</tr>
<tr>
<td>TW Vacuum Box 14</td>
<td></td>
</tr>
</tbody>
</table>

### Abs. Causes

<table>
<thead>
<tr>
<th>TW Vacuum Box 15</th>
</tr>
</thead>
<tbody>
<tr>
<td>Post Former Dryness</td>
</tr>
<tr>
<td>Wire Section Drive Power</td>
</tr>
<tr>
<td>Couch Roll Dryness</td>
</tr>
<tr>
<td>Wire Combining Roll Amps</td>
</tr>
<tr>
<td>TW Vacuum Box 14</td>
</tr>
<tr>
<td>TW Vacuum Box 10</td>
</tr>
</tbody>
</table>

- Conclusion after examining correlations from all TL variables: too much vacuum is being applied on the TL. This is increasing drive power consumption for no net gain in dryness.
Tests on Headbox Variables

- Process response tests were applied to the following TL and BL headbox variables:
  - Rush/Drag
  - Slice Opening

- Both have a significant effect on pre-former dryness, wire section power, sheet moisture, weight and former total flow.

- In general, applying more drag:
  - Increases pre-former dryness.
  - Decreases sheet moisture and basis weight.
  - Decreases total former flow.
  - Doesn’t change the wire section power significantly.

- Opening the slice gap:
  - Decreases pre-former dryness.
  - Decreases sheet moisture and basis weight.
  - Increases total former flow.
  - Increases wire section power.
Process Response Tests
BL Headbox Rush/Drag and Slice Opening

The influence on sheet dryness is not as clear. Initial steps had a good response, but later steps did not.

Rush/drag has a strong effect on power, moisture and former flow. When rush/drag is reduced moisture and total flow both increase.

Slice gap has the opposite effect. Opening the slice increases former flow but reduces sheet moisture.
Process Response Tests
Headbox Correlations

Bottom Layer

Rush/Drag

<table>
<thead>
<tr>
<th>Abs. Causes</th>
<th>5255.ME BL Headbox Rush/Drag SP</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rush/Drag</td>
<td>Abs. Effects</td>
</tr>
<tr>
<td>Headbox</td>
<td>Rush/Drag</td>
</tr>
<tr>
<td>Pre Former</td>
<td>Dryness</td>
</tr>
<tr>
<td>Total</td>
<td>Former Dryness</td>
</tr>
<tr>
<td>Flow</td>
<td>Sheet</td>
</tr>
<tr>
<td>Wire Sect</td>
<td>Drive Power</td>
</tr>
<tr>
<td>Wire Roll</td>
<td>Dryness</td>
</tr>
<tr>
<td>Post Former</td>
<td>Dryness</td>
</tr>
</tbody>
</table>

Large effect on pre-former dryness, flow and moisture

Slice Gap

<table>
<thead>
<tr>
<th>Abs. Causes</th>
<th>4965.ME BL Slice Gap SP</th>
</tr>
</thead>
<tbody>
<tr>
<td>Slice Gap</td>
<td>Abs. Effects</td>
</tr>
<tr>
<td>TL Slice</td>
<td>Gap SP</td>
</tr>
<tr>
<td>Wire Sect</td>
<td>Drive Power</td>
</tr>
<tr>
<td>Wire Roll</td>
<td>Dryness</td>
</tr>
<tr>
<td>Sheet</td>
<td>Moisture</td>
</tr>
<tr>
<td>Pre Former</td>
<td>Dryness</td>
</tr>
<tr>
<td>Post Former</td>
<td>Dryness</td>
</tr>
</tbody>
</table>

Very large effect on pre-former dryness, flow and power

Top Layer

Rush/Drag

<table>
<thead>
<tr>
<th>Abs. Causes</th>
<th>5055.ME TL Headbox Rush/Drag SP</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rush/Drag</td>
<td>Abs. Effects</td>
</tr>
<tr>
<td>TL Headbox</td>
<td>Rush/Drag</td>
</tr>
<tr>
<td>Wire Combing Roll Amps</td>
<td></td>
</tr>
<tr>
<td>Top Wire</td>
<td>Combing Roll Amps</td>
</tr>
<tr>
<td>Wire Sect</td>
<td>Drive Power</td>
</tr>
<tr>
<td>Wire Roll</td>
<td>Dryness</td>
</tr>
<tr>
<td>Post Former</td>
<td>Dryness</td>
</tr>
<tr>
<td>Sheet</td>
<td>Moisture</td>
</tr>
<tr>
<td>Pre Former</td>
<td>Dryness</td>
</tr>
</tbody>
</table>

Large effect on power; small effect on couch dryness nothing on sheet moisture

Slice Gap

<table>
<thead>
<tr>
<th>Abs. Causes</th>
<th>4955.ME TL Slice Gap SP</th>
</tr>
</thead>
<tbody>
<tr>
<td>TL Slice</td>
<td>Gap SP</td>
</tr>
<tr>
<td>Wire Sect</td>
<td>Drive Power</td>
</tr>
<tr>
<td>Wire Roll</td>
<td>Dryness</td>
</tr>
<tr>
<td>Sheet</td>
<td>Moisture</td>
</tr>
<tr>
<td>Pre Former</td>
<td>Dryness</td>
</tr>
<tr>
<td>Post Former</td>
<td>Dryness</td>
</tr>
</tbody>
</table>

Large effect on power only
Process Modelling

- The set of process response tests and selected running data has been used to build a preliminary process model.
  - This model is preliminary in that it doesn't take into account changes in process gain due to grade and basis weight (further tests would be required).
- As inputs, the model uses all of the serviceable forming table vacuums, headbox parameters, the bottom layer drainage rate transmitter and the measured steam flow to the machine.
  - It predicts changes in the online sheet dryness, wire section power load and MD moisture.
- The model was then used to:
  - Determine which vacuums and other variables have the strongest influence on moisture.
  - Quantify the effect of freeness changes on drying.
  - Build a simulation to evaluate various optimisation strategies.
The model provides a new prediction every 20 seconds. Each bar in the histogram represents 20 seconds. Total response time = 6 mins.

Observation: slice and rush/drag affect moisture, but much of the effect appears to dissipate (short circulation balancing?)

Vac box 11 appears the most powerful. However, it was tested at a heavier basis weight, so this may have an influence.

All BL (BW) vac boxes have the same type of effect: more vacuum decreases pre-former dryness, increases couch dryness and decreases sheet moisture.

<table>
<thead>
<tr>
<th>Cause Variables (Inputs)</th>
<th>Effect Variables (Outputs)</th>
</tr>
</thead>
<tbody>
<tr>
<td>BW Vacuum Box 11A (kPa)</td>
<td>Pre-former Dryness (%)</td>
</tr>
<tr>
<td>BW Vacuum Box 10A (kPa)</td>
<td>Post-former Dryness (%)</td>
</tr>
<tr>
<td>BW Vacuum Box 9A (kPa)</td>
<td>Pre-couch Dryness (%)</td>
</tr>
<tr>
<td>BW Vacuum Box 9B (kPa)</td>
<td>Sheet Moisture (%)</td>
</tr>
<tr>
<td>BW Vacuum Box 9D (kPa)</td>
<td>Wire Section</td>
</tr>
<tr>
<td>TL Slice Gap SP (mm)</td>
<td>-0.06</td>
</tr>
<tr>
<td>BL Headbox Rush/Drag SP (m/min)</td>
<td>0.1067</td>
</tr>
<tr>
<td>TL Headbox Rush/Drag SP (m/min)</td>
<td>0.013</td>
</tr>
<tr>
<td>TL Slice Gap SP (mm)</td>
<td>0.045</td>
</tr>
<tr>
<td>BL Headbox Rush/Drag SP (m/min)</td>
<td>-0.017</td>
</tr>
<tr>
<td>TL Headbox Rush/Drag SP (m/min)</td>
<td>0.013</td>
</tr>
<tr>
<td>BL Headbox Rush/Drag SP (m/min)</td>
<td>-0.017</td>
</tr>
<tr>
<td>TL Headbox Rush/Drag SP (m/min)</td>
<td>-0.017</td>
</tr>
<tr>
<td>TL Headbox Rush/Drag SP (m/min)</td>
<td>-0.017</td>
</tr>
</tbody>
</table>
Process Model – Part B
Former and TL Vacuums

Effect Variables (Outputs)

<table>
<thead>
<tr>
<th>Cause Variables (Inputs)</th>
<th>Direction</th>
<th>Pre-former Dryness (%)</th>
<th>Post-former Dryness (%)</th>
<th>Pre-couch Dryness (%)</th>
<th>Sheet Moisture (%)</th>
<th>Wire Section Power (kWhr)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Former 2nd Comp Vac SP (MWC)</td>
<td>Up</td>
<td>0.137</td>
<td>0.144</td>
<td>-0.364</td>
<td>31.56</td>
<td></td>
</tr>
<tr>
<td>Former 3rd Comp Vac SP (MWC)</td>
<td>Up</td>
<td>0.086</td>
<td>0.026</td>
<td>-0.030</td>
<td>-1.905</td>
<td></td>
</tr>
<tr>
<td>TW Vacuum Box 15 (kPa)</td>
<td>Up</td>
<td>-0.030</td>
<td>-0.054</td>
<td>-10.204</td>
<td></td>
<td></td>
</tr>
<tr>
<td>TW Box 10A-14 Av Vacuum (kPa)</td>
<td>Up</td>
<td>0.014</td>
<td>-0.054</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>All K12 Vac Controller OP (%)</td>
<td>Down</td>
<td>-0.026</td>
<td>No Data</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Total Steam Flow</td>
<td>Up</td>
<td></td>
<td>-0.003</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

The second compartment has a pronounced effect on sheet moisture, but the third compartment has essentially no effect.

The TL/TW master valve has a small effect on sheet moisture and a fairly large effect on power as well.

Total steam use is included for optimisation purposes.
This trend presents the model predictions for the BL Rush/Drag tests. Red = Prediction. Blue/Green = Process Variable.
Process Optimisation Scenarios

- A process simulator and Model Predictive Controller have been constructed from the model.
- The simulator runs ten times faster than real-time. This allows different control and optimisation "scenarios" to be tested and evaluated quickly:
  - **Scenario 1: Electrical Energy Saving**
    - Maintain the same pre-couch dryness and steam consumption.
    - Save 10% in total electrical energy.
    - Maintain at least 8200 l/min former flow and control MD moisture to SP.
  - **Scenario 2: Steam Energy Saving.**
    - Allow pre-couch dryness to move as required.
    - Save 10% in steam energy.
    - Maintain at least 8200 l/min former flow and control MD moisture to SP.
Process Optimisation Scenarios

Scenario 1: Electrical Energy Saving

1. The simulation is set up with the same values as a recent 140 gsm run.

2. The wire section power target is reduced by 10%.

3. The system immediately releases vacuum from the TL but increases the former 2nd & 3rd compartment vacs.

4. Most BL vacuums are released slightly, increasing dryness into the couch and saving energy.

5. Given these conditions there is easily sufficient headroom to achieve a 10% energy saving.
Process Optimisation Scenarios

Scenario 2: Steam Energy Saving

1. In this simulation we introduce total steam flow and give it a target of 10% below the initial value.

2. Most BL vacuums are released slightly.

3. This increases couch dryness, allowing steam to be reduced.

4. A 9.6% steam saving is achieved. As a bonus, electrical energy also drops by 2%.

5. In the final part of this scenario another 10% saving is attempted. This causes all the vacuums to saturate. This would not be achievable in reality.
Recommendations 1: Vacuums and Headbox Parameters that Affect Drainage

The study has investigated which wet-end, headbox and wire-section variables have an influence on drainage and sheet moisture:

- All tested vacuums have an influence on drainage, but not all of them have a corresponding influence on sheet moisture:
  - Too much vacuum in the Bottom Layer (BL) forming table boxes has a detrimental effect on drainage. Early high vacuum increases pre-former dryness but reduces pre-couch dryness and increases both sheet moisture and wire-section drive load.
  - Similarly on the Top Layer (TL) too much vacuum is presently being applied at the expense of electrical energy efficiency.
  - Vacuums after the former also have an effect on dryness but do not have an effect on sheet moisture. This suggests a buffering effect in the press-section.
- As expected, each headbox's slice gap has a large impact on sheet moisture. This response tends to dampen out as the short-circulation system balances out. The TL rush/drag has a surprisingly strong effect on wire section power and pre-couch dryness.
Recommendations 2: Optimal Strategy to Maximise Sheet Dryness

- Optimal settings: use as little vacuum on the forming table as possible.
  - The wet or activity line should be just before the former's lead roll.
  - The second compartment should have a reasonable amount of vacuum applied (1.2-1.6 MWC).
  - The third compartment should have a low vacuum as it increases drive power consumption unnecessarily.
  - The TL vacuums should be released as much as possible.
  - It would be worth experimenting with more drag on the TL headbox.
Towards Further Reduction of Energy Use in Paper Making: Better Control of the Dryer (1)

We propose two approaches to better control of the dryer:

1. Use all the available dryer variables to better control the drying of the sheet
   - The traditional regulatory approach to controlling a paper machine dryer usually uses a three term (PID) loop:
     • driven by the difference between measured and target sheet moisture
     • control action is cascaded to operate on steam pressures in 3 – 7 dryer sections, aiming to meet the moisture target
   - A multivariable APC approach to dryer control could be based on building separate models of the effect on sheet moisture of:
     • the steam pressure in each dryer section
     • the differential pressures across each dryer section
     • the condensate recovery rate from each dryer section (if independent)
   - Differential pressures and condensate recovery rates are seldom used in closed loop dryer control schemes: neither operating practice nor the literature provide clear guidelines about how to use these variables to optimise dryer performance
   - A control system with closed loops around steam pressure alone will be ignoring some important variables of influence on dryer operation
Towards Further Reduction of Energy Use in Paper Making: Better Control of the Dryer (2)

2. Optimise the operation of the dryer hood
   - The traditional regulatory approach to control of the hood environment of a paper machine dryer also usually uses three term (PID) loops
   - Actually the hood is a multivariable system requiring real time optimisation to minimise energy use
   - In a current project, we have found modellable effects on sheet moisture and dryer steam use of variables such as
     • Inlet air flowrates, on both the wet side and the dry side
     • Exhaust air temperature targets
     • Exhaust air humidity targets
   - Some early analysis of these opportunities is reported in the paper
Conclusion

• A significant reduction in the energy consumed in paper making is possible using Advanced Process Control (APC). Methodology:
  - Model the machine as a multivariable process
  - Use this model to design a multivariable model predictive controller
  - Run the controller with powerful real-time optimisation functionality

• Evidence to date shows there are good prospects of reducing the energy used in paper making by at least 20%:
  - 10% reduction from better control of wet end stability
  - Up to another 10% reduction by better control of sheet drainage
  - There are prospective further benefits, not yet quantified, arising from:
    • Better control of the dryer, using all available dryer variables
    • Optimisation and better regulation of the dryer hood